

Abstract

In this paper the use of fuzzy logic to control the position of anti aircraft tube is offered. By processing the received information from radar the action of tracking the target is done. It is supposed that the anti aircraft is fixed on a moving leg. In this form two completely separated controller has been designed, that the first controller is to tracking the target permanently and the second controller is to stabilizing the anti aircraft tube against completely sudden vibration from leg movement.

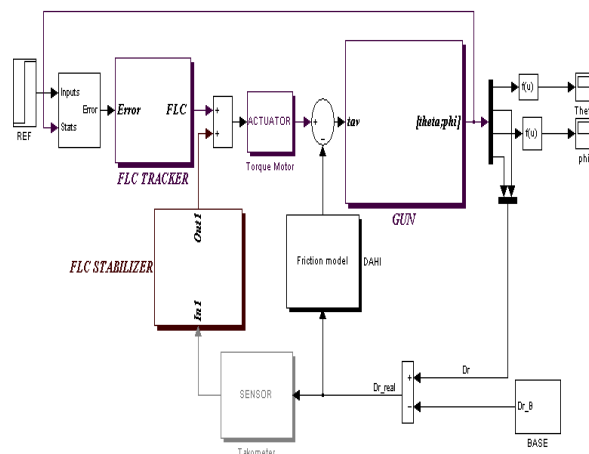
Keywords: tracker, fuzzy controller, anti aircraft, stabilizing

Introduction

Target tracking in the long past has been one of the most important case in the military crafts. tracking and following the object or path can be done manually or automaticly. A target tracking means determine the output torques of motors proportional by new states of lateral and vertical angle. In this systems by target movement in the space, two motors regulate new state based on target's position that this process is done continuously.

Cloosloop system parts

The system closeloop parts and controllers form is shown in figure(1). the anti aircraft is a nonlinear and time invariant system that its



nonlinearity is rather
 Fig. 1. the cloos loop system and controller

high so practically the classic controllers for moving type is difficult. According to amount of comparative moving between base and gun variations of lateral and vertical angles in every moment has been determine. this comparative movement is applied to a tachometer. Output of tachometer applied to another fuzzy controller that its duty is stabilizing of gun.

The motors have a transfer function by equation (1) that in this $\omega_c = 6338.8$ and $k_c = 0.1$

$$H_m(S) = \frac{k_c \cdot \omega_c}{s + \omega_c} \quad -10 \leq I_{in} \leq 10 \quad (1)$$

System dynamic equations is simplified as they have been in equation(2).

$$\theta'' = \frac{-3g}{2L} \cdot \sin \theta - 0.5\phi'^2 \cdot \sin 2\theta - \frac{3f_a}{m.L^2} \cdot \theta' + \frac{3\tau_a}{m.L^2} \cdot i_a \quad (2)$$

$$\phi'' = -\theta' \cdot \phi' \cot g\theta - \frac{3f_e}{m.L^2 \cdot \sin \theta} \cdot \phi' + \frac{3\tau_e}{m.L^2 \cdot \sin \theta} \cdot i_e$$

In order to get the system state space form, state variables are defined as they have been in equation(3).

$$X_1 = \theta, X_2 = \theta', X_3 = \phi, X_4 = \phi' \quad (3)$$

There fore equation(4) is produced.

$$\begin{aligned}
 (4) \\
 X_1' &= X_2 \\
 X_2' &= \frac{-3g}{2L} \cdot \sin x_1 - 0.5X_4^2 \cdot \sin 2x_1 - \frac{3f_a}{m.L^2} \cdot X_2 + \frac{3\tau_a}{m.L^2} \cdot i_a \\
 X_3' &= X_4 \\
 X_4' &= -X_2 \cdot X_4 \cot g\theta - \frac{3f_e}{m.L^2 \cdot \sin \theta} \cdot X_4 + \frac{3\tau_e}{m.L^2 \cdot \sin x_1} \cdot i_e
 \end{aligned}$$

As you see the anti aircraft is a 4 degree system with two inputs and two outputs.

In this system the tachometer transfer function is as in the form of equation(5).

$$H_t(s) = \frac{\omega_t^2}{s^2 + 2\xi_t \omega_t s + \omega_t^2} \quad (5)$$

$$\omega_t = 2\pi(150) \quad \xi_t = 0.7$$

The friction model that has been used has difrentional equation in the form of equation(6).

$$\begin{aligned}
 \frac{d\tau_f}{dt} &= \frac{d\theta_{Rel}}{dt} \cdot \gamma \cdot [(\tau_f) (\text{sgn}(\theta'_{Rel}) - \tau_{f0})]^2 \quad (6) \\
 \tau_{f0} &= 0.5 \max(\tau_f)
 \end{aligned}$$

That τ_f is friction torque, θ_{Rel} is relative rotational speed between base and gun and t is reagent time. γ is a factor that show maximum curve ramp of τ_f and it is related to the material of contacte surface.

Controlers

Tracker fuzzy controller

In this section infact we have worked on a system with out platform consideration. We want to control a fixed anti aircraft. our opration criteria are error and variations of error in the tracking loop, Based on a trial and error method[1,2].The tracker controller rule base was determinate. This has been done according to the global knowledge about this system.

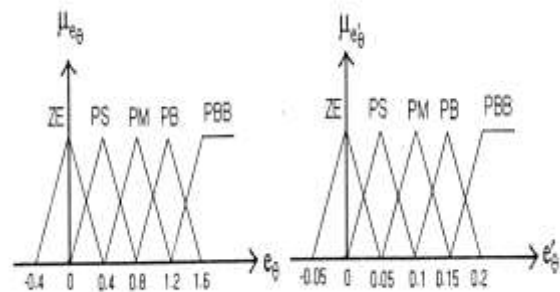


Fig.2. membership functions of vertical angle error and error variations

Membership functions that we have choosed for this refrence sets are all triangle type. For tracking error and error changes of vertical angle 5 linguistic variables are defined. this 5 variables are defined on the reference set e_θ, e'_θ are:

- ZE = zero
- PS = positive and small
- PM = positive and medium
- PB = positive and big
- PBB = positive and very big

Membership functoins of error and error variations of vertical angle are shown in figure(2).

Therefore we have 25 control rules that shown in table(1). In the otherhand output of fuzzy controller for control the vertical angle is I_a that it is the current of armicher of the motor for control the vertical angle (θ).

According to motor's behavior 6 linguistic variables as follows are defined on the I_a reference set:

- ZE = zero
- PSS = positive and very small
- PS = positive and small
- PM = positive and medium
- PB = positive and big
- PBB = positive and very big

Table.1. rule base for vertical angle control

error	variations of error				
	ZE	PS	PM	PB	PBB
ZE	ZE	PSS	PSS	PS	PB
PS	PS	PS	PS	PM	PM
PM	PM	PM	PM	PB	PB
PB	PB	PB	PB	PB	PBB
PBB	PBB	PBB	PBB	PBB	PBB

Similary rule base for angle tracking loop control (ϕ) is determined. Here also membership functions are triangular type and again 5 linguistic variables for reference sets e_ϕ, e'_ϕ are determined:

- N = negative
- ZE = zero
- PS = positive and small
- PM = positive and medium

PB = positive and big

That are shown in the table(2).

In the same way fuzzy controller output of this loop is I_e that is current motor's armature for control the lateral angle that 7 linguistic variables are defined on its reference sets:

- N = negative
- NZ = negative and nearby zero
- ZE = zero
- PZ = positive and nearby zero
- PS = positive and small
- PM = positive and medium
- PB = positive and big

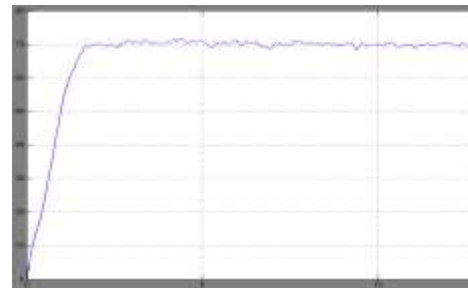
Table 2.rule base for lateral angle control

error	variations of error				
	N	ZE	PS	PM	PB
N	N	N	N	ZE	ZE
ZE	NZ	ZE	ZE	PZ	PZ
PS	PZ	PS	PS	PS	PM
PM	PS	PS	PM	PM	PM
PB	PM	PM	PB	PB	PB

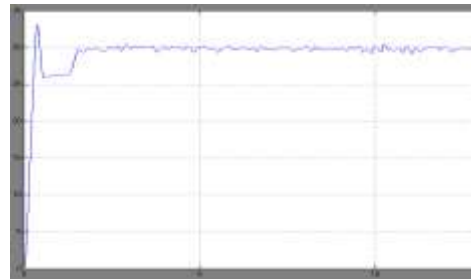
Stabilizer fuzzy controller

The ship angular movements are decomposed into vertical angle and lateral angle (θ, ϕ) [5,6]. These two will be measured by ship horizontal gyroscope. In the simulation these two components be assumed two quite separated random variables. According to the military crafts power spectrum density of this random variable can be reagent noise source of this components $\theta_{Base}, \phi_{Base}$. in the worst conditions create 12(deg/sec) to 15 (deg/sec) in the ship position. Here also we use the error and error changes for rules regulation. Fuzzy rule for correction the lateral angle I_e is as below:

- If e_t is ZE , e'_t is ANY Then I_a is ZE
- If e_t is PB , e'_t is PB Then I_a is NB
- If e_t is PM , e'_t is ANY Then I_a is NM
- If e_t is PS , e'_t is PS Then I_a is NS
- If e_t is NS , e'_t is PS Then I_a is ZE
- If e_t is NM , e'_t is PM Then I_a is PS
- If e_t is NB , e'_t is NB Then I_a is PB
- If e_t is NB , e'_t is NS Then I_a is PM

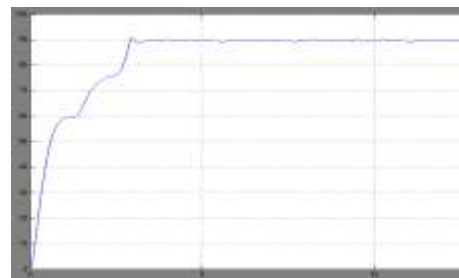


Phi



teta

Fig.5. system response with controlers for $\theta = 30^\circ, \phi = 70^\circ$



teta



Phi

Fig.5. system response with controlers for $\theta = 90^\circ, \phi = 170^\circ$

If e_t is NB , e'_t is PB Then I_a is PS

And also fuzzy rules to correct the vertical angle is:

If e_p is ZE , e'_p is any Then Ia is NB
If e_p is NB , e'_p is any Then Ia is PB
If e_p is PM , e'_p is any Then Ia is NM
If e_p is NM , e'_p is any Then Ia is PM

System response with controllers for the moment position is shown in figure(5).

It is seen that the responses of tracking the given angles with negligible error. Also for moment position the system responds with controllers shown in figure(6).

Conclusion

In this simulation clearly it was seen that with forced constant torque of motor to gun the vertical angle will increase partly. After that the equilibrium between resistant and motive torque was created, in the specified point amount of vertical angle reach to a steady state. As well as this system is nonlinear

And nontimeinvariant, because the amount of nonlinearity is rather high thus the use of the classic controller for control

the movable type will be difficult. But with fuzzy control we can control it by suitable way.

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